

Transitioning ultrasonic ply-tracking algorithms from academia to industry

Robert A Smith¹,

Professor of NDT and High Value Manufacturing

Director of the UK Research Centre in NDE

Luke Nelson¹, Rostand Tayong¹ and Laura Maybury²

¹Dept. of Mechanical Engineering, University of Bristol, BS8 1TR, UK.

²University of the West of England, Bristol, UK

Acknowledgements

- Prof Paul Wilcox
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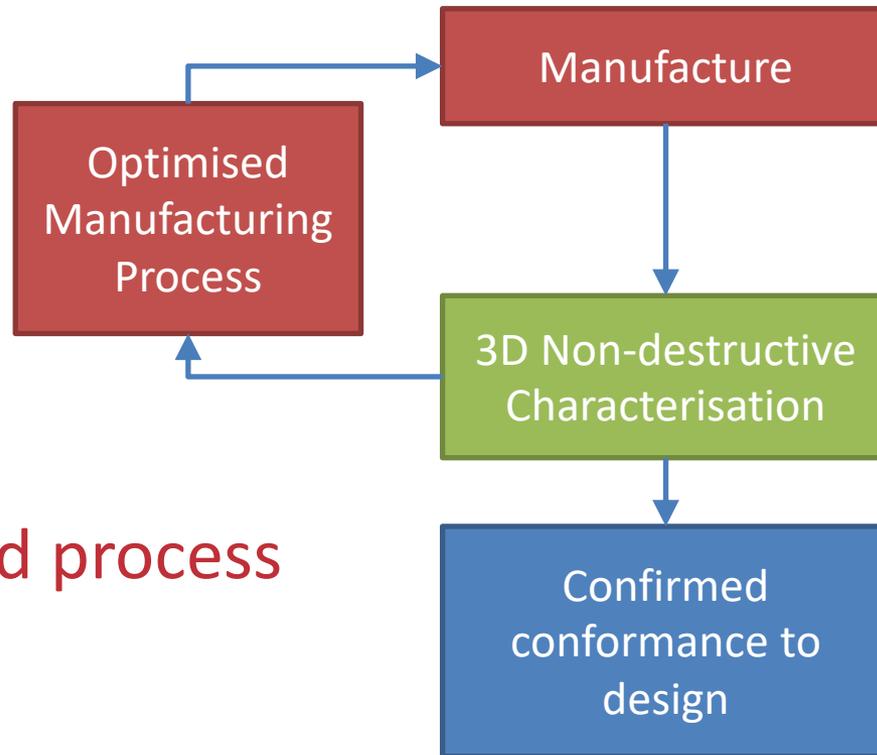


EPSRC

Engineering and Physical Sciences
Research Council

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- Introduction
 - Stage 1: Analytic-signal and instantaneous parameters
 - Stage 2: Ply tracking
 - Stage 3: Ply wrinkling
 - Stage 4: In-plane waviness, Stacking sequence, 2D and 3D woven composites
 - Transitioning algorithms to industry
 - Conclusions
-

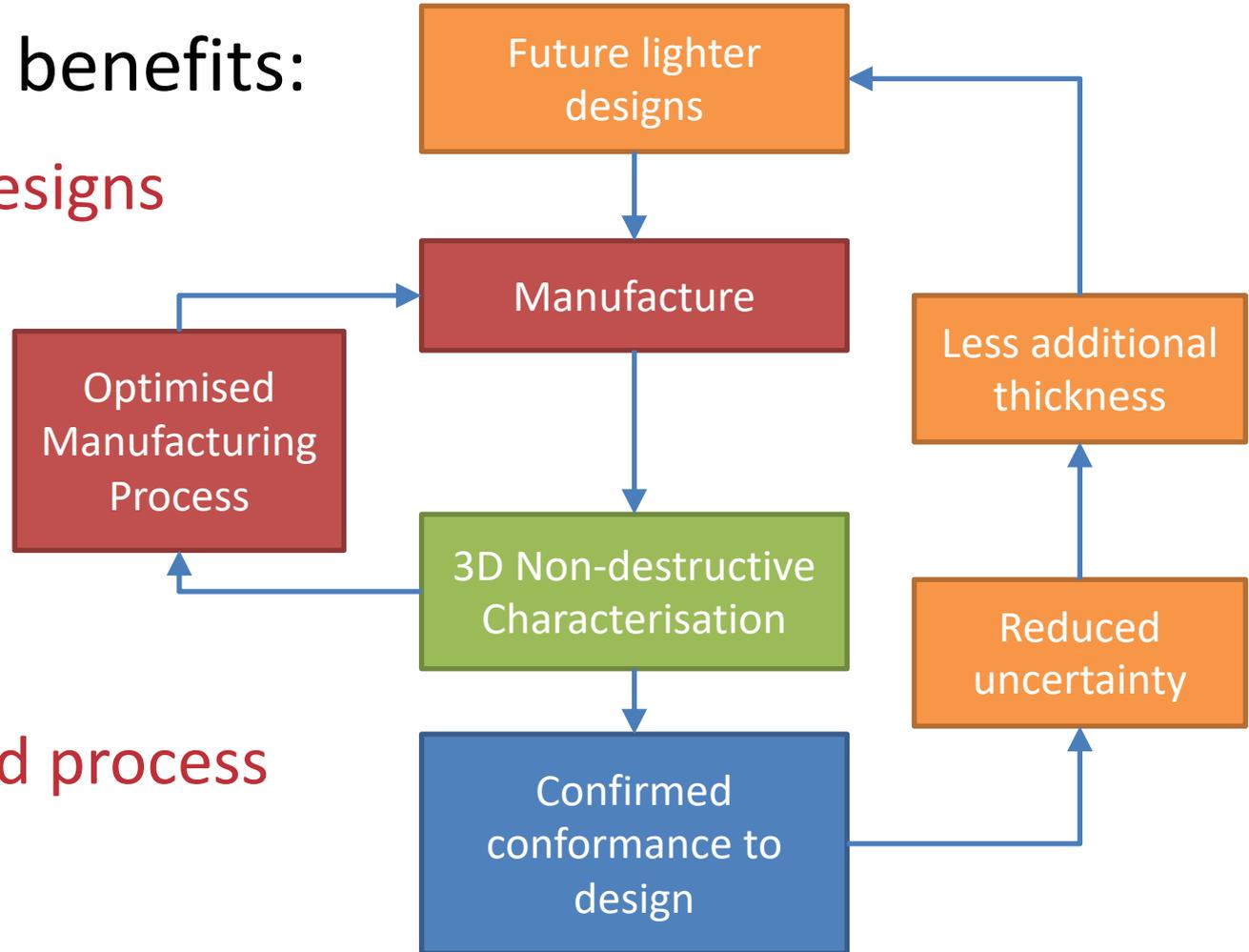
- Long-term benefits:



- Optimised process

- Long-term benefits:

- Lighter designs



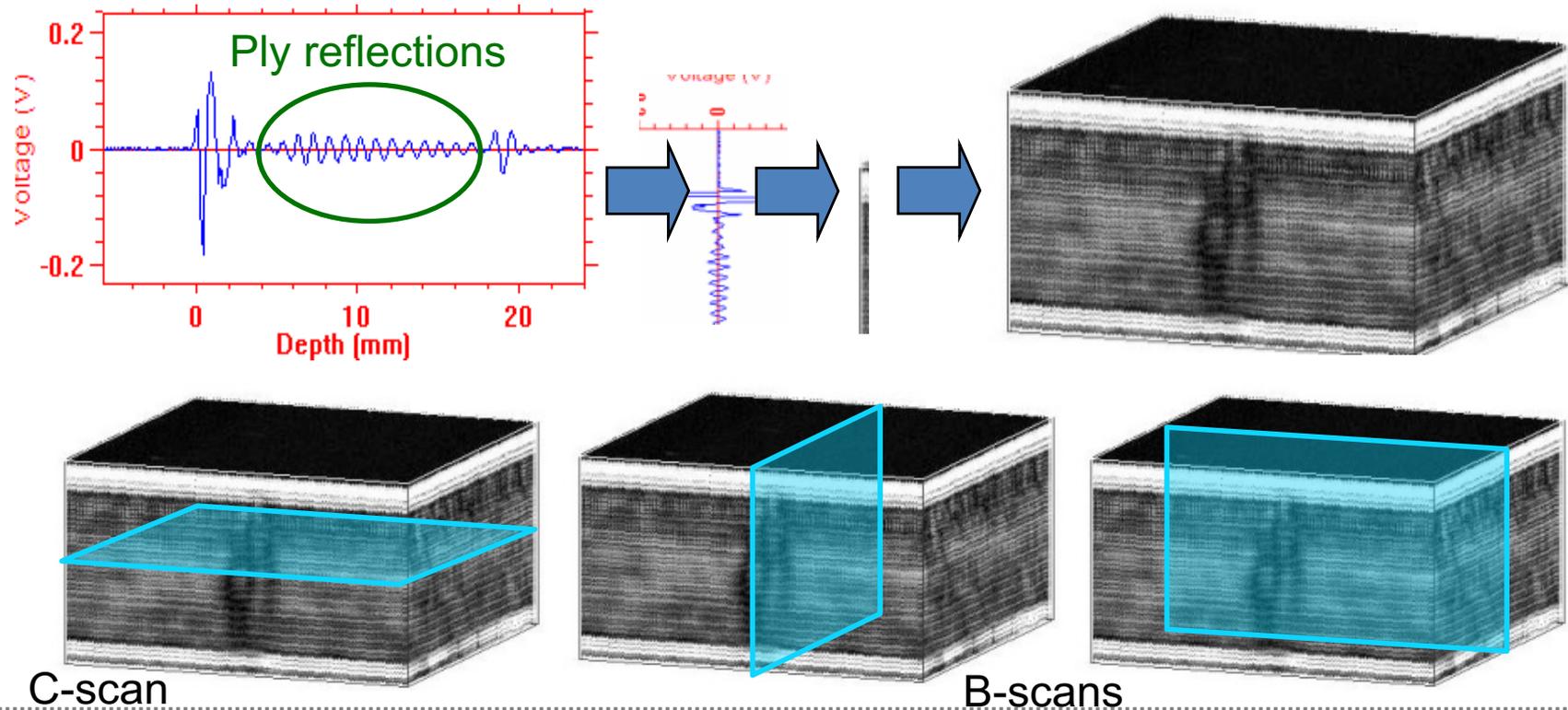
- Optimised process

- Using MTC's Algorithm Deployment Support Service
 - *Transitions Software Engineering Documents*
 - **Currently transitioning into supply chain:**
 - Stage 1: Analytic-signal and instantaneous parameters
 - Stage 2: Ply tracking
 - Stage 3: Out-of-plane ply orientation and wrinkle mapping
 - **Through: Ultrasonic Sciences Ltd, Wavelength NDT/UTEX**
 - **Planning the project consortium for:**
 - Stage 4: 2D woven composite classification and mapping
 - **Through DolphiTech (all four stages) for DolphiCam2.**

Stage 1: Analytic-signal and instantaneous parameters

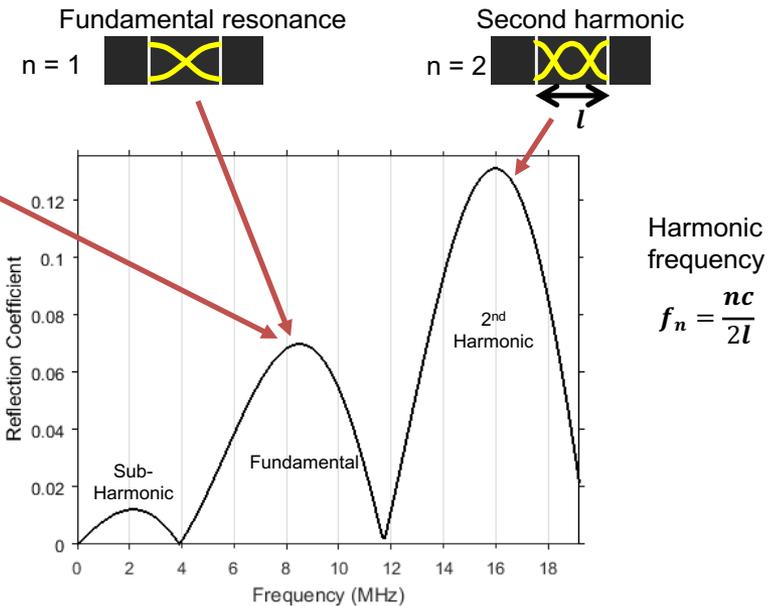
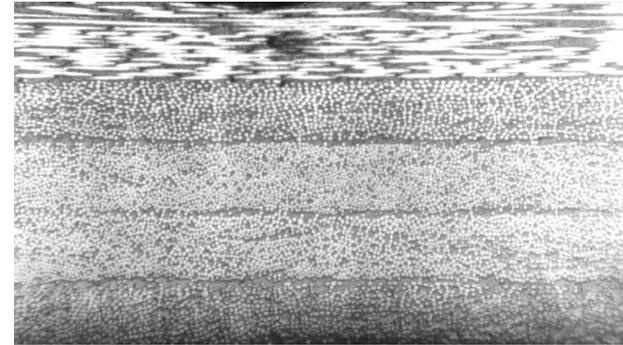
Ultrasound 3D data sets

- Normal incidence focused probe – focused on mid-plane

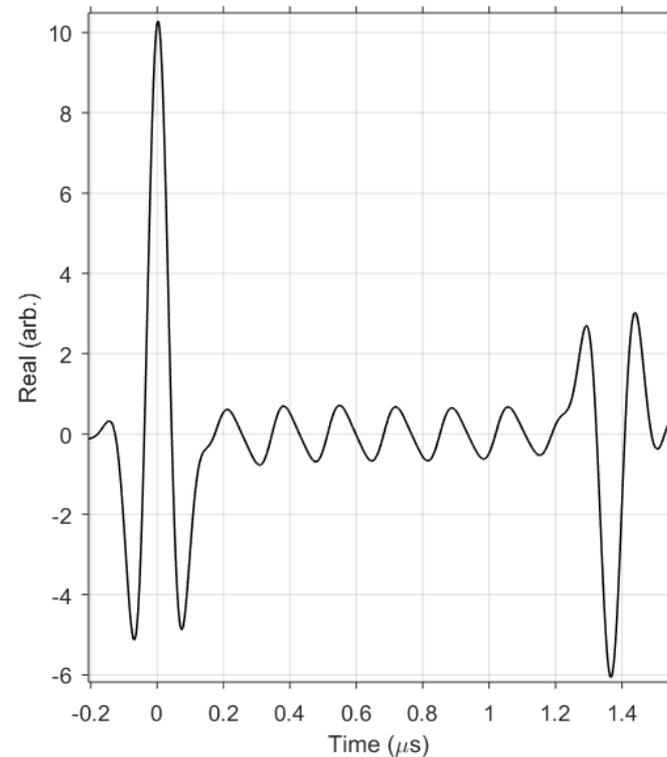
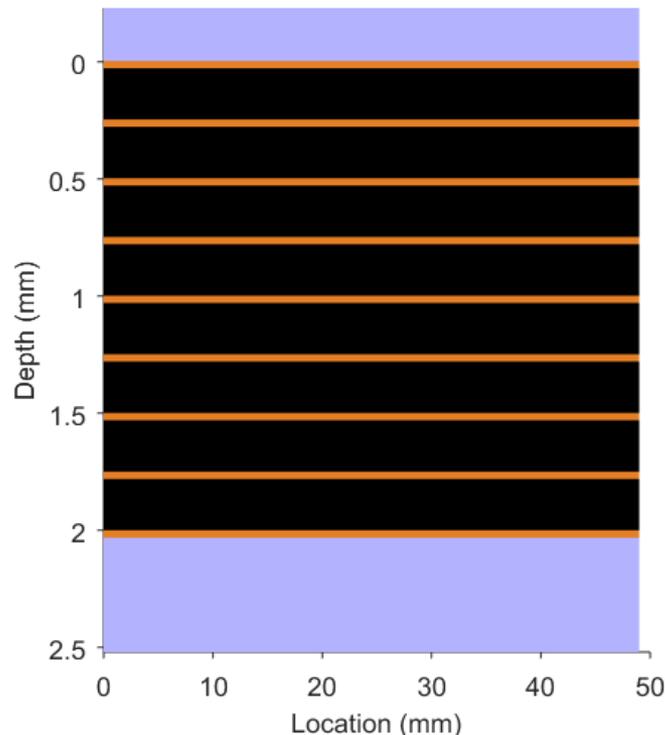


- CFRP

- Resin layers reflect
- Interference between reflections
- Weak resonances, eg
 - 8 MHz for 0.189 mm plies
- Resonances disrupted by:
 - Ply thickness variations
 - Material property variations
- Localised response
 - Reflections are only weak



- 8 plies in water – normal incidence pulse-echo

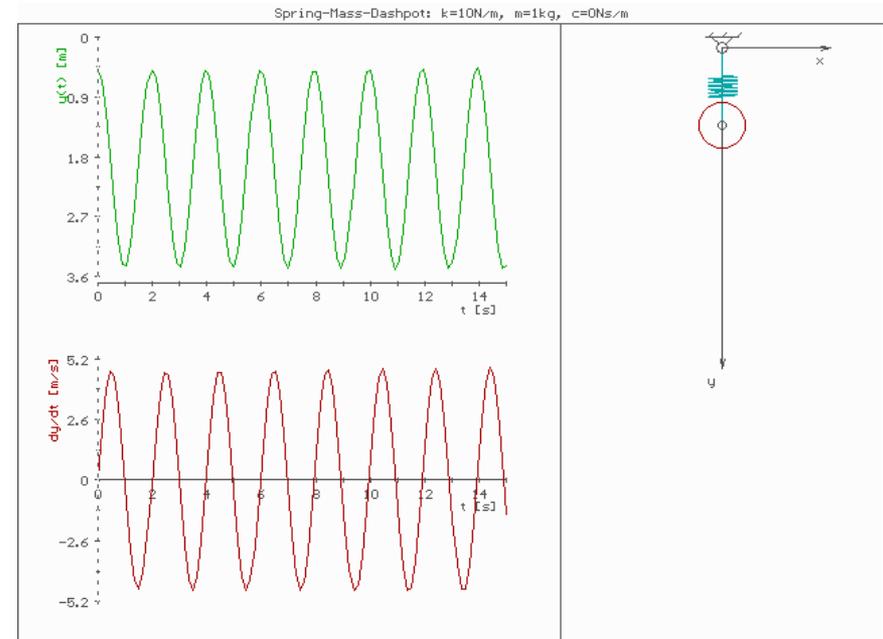
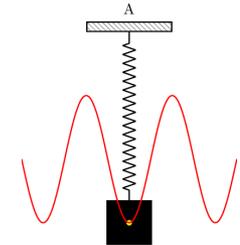
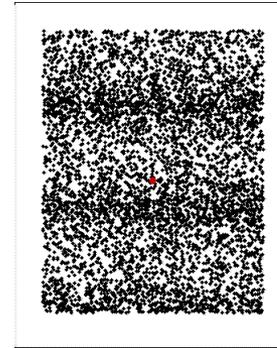


Measured parameter is usually acoustic pressure (proportional to particle velocity)

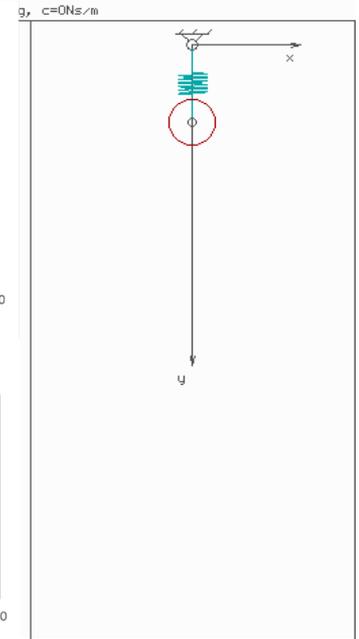
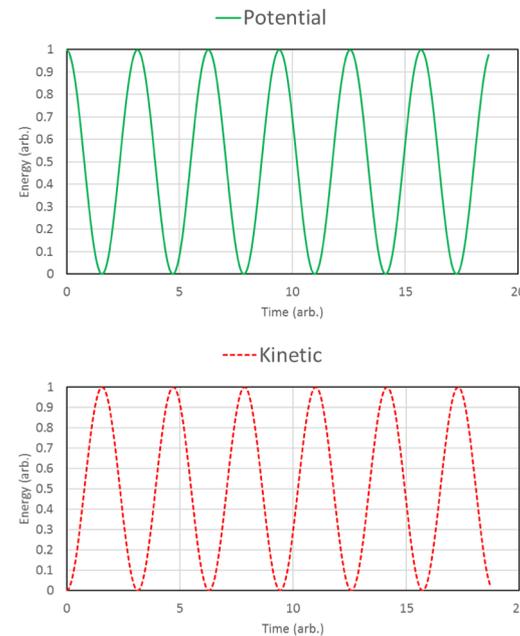
- Analytic signals
 - Mass-spring analogy

- Particle Displacement.

- Particle Velocity
 - 90° ($\pi/2$) out of phase with displacement



- Analytic signals
 - Mass-spring analogy
 - Energy transfer
- Particle Displacement.
 - Potential energy = $\frac{1}{2}kx^2$
- Particle Velocity
 - Kinetic energy = $\frac{1}{2}mv^2$



- Analytic Signal $a(t)$

$$a(t) = A(t)e^{i\phi(t)}$$

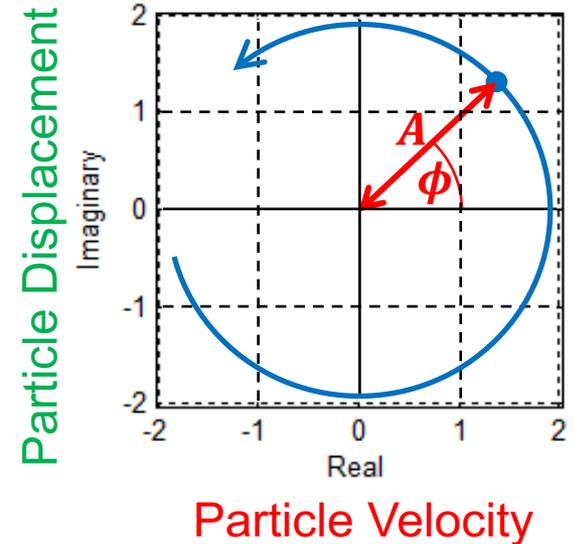
where: $A(t)$ is instantaneous amplitude

$\phi(t)$ is instantaneous phase

$\frac{1}{2\pi} \frac{d\phi}{dt}$ is instantaneous frequency

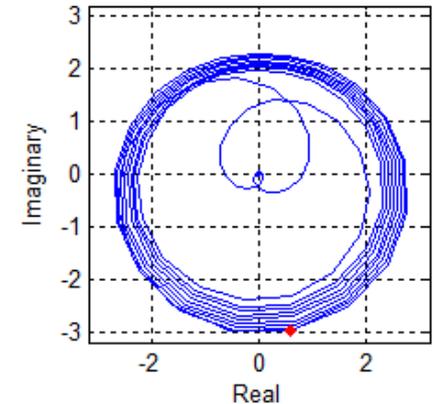
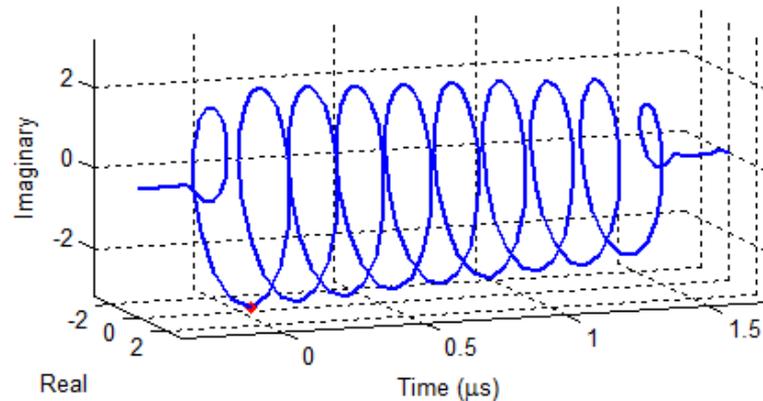
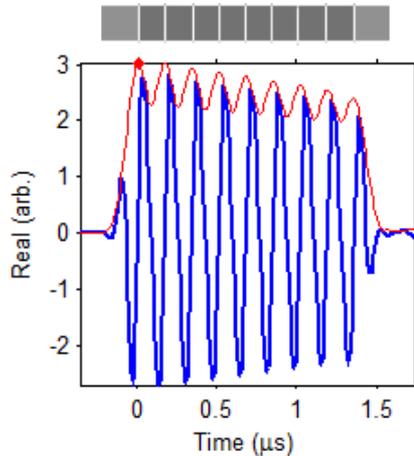
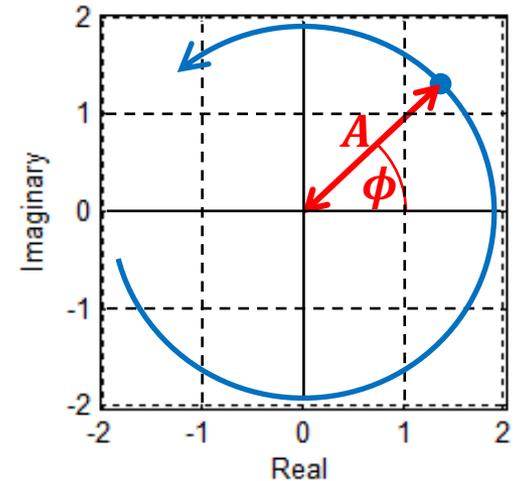
(local phase gradient)

- Use a **Hilbert Transform** to create imaginary part from real waveform.



$$a(t) = A(t)e^{i\phi(t)}$$

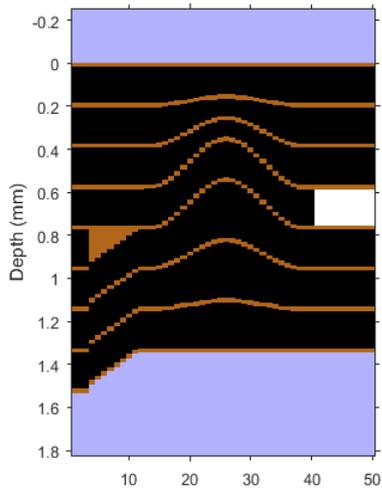
- At resonance, a particular phase is *locked* to resin layers between plies.



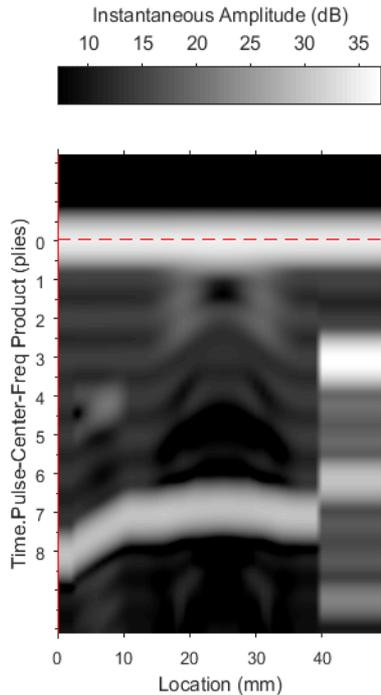
8-ply CFRP laminate, 0.25 mm ply spacing, between matching layers

- Simulated ply drop, wrinkle and delamination

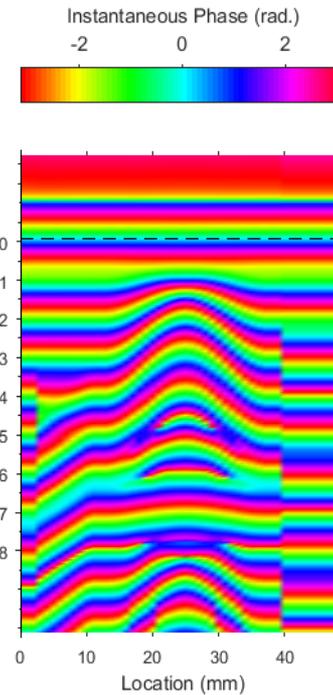
Simulation



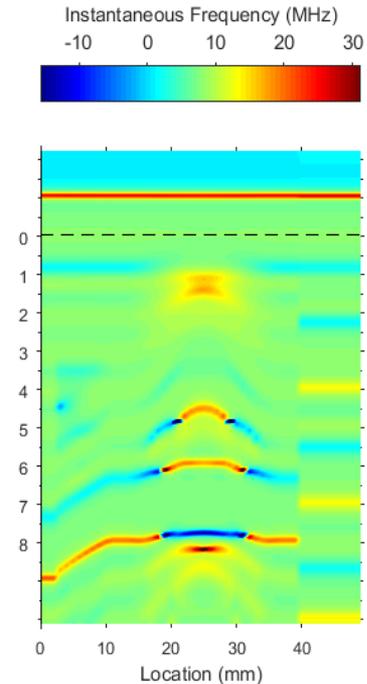
Instantaneous
Amplitude



Instantaneous
Phase

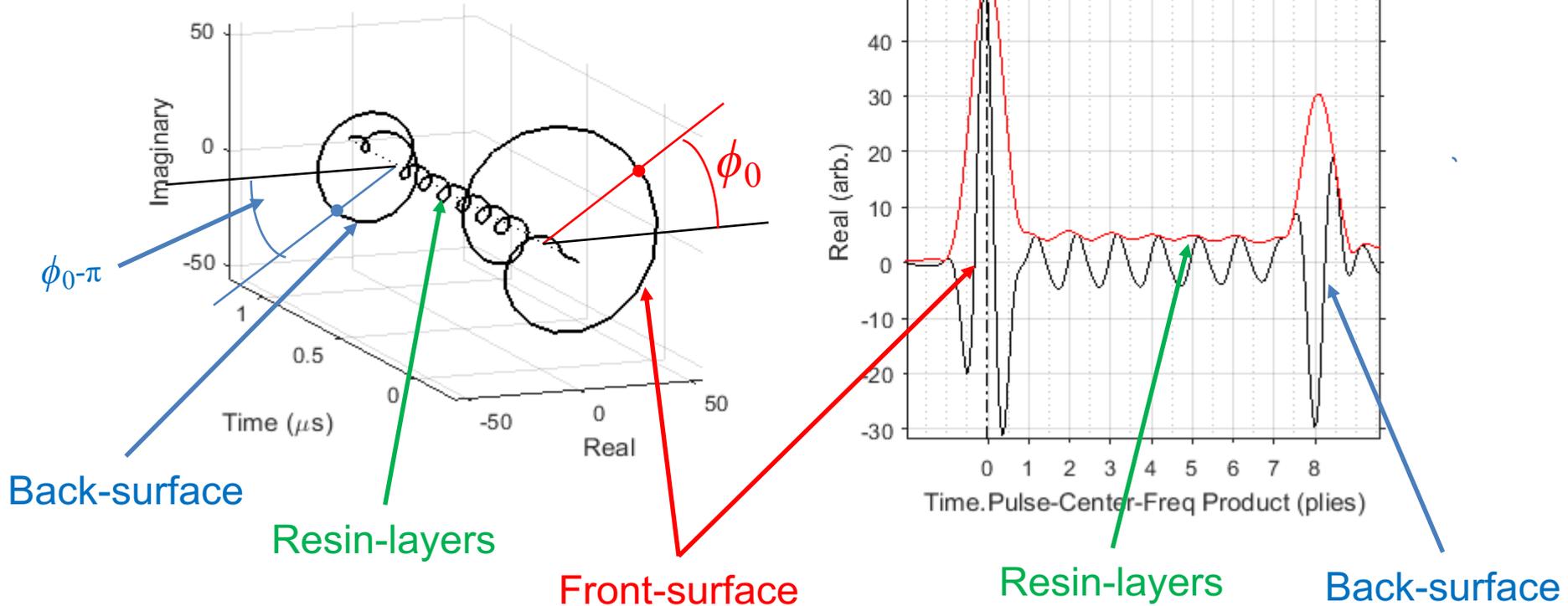


Instantaneous
Frequency

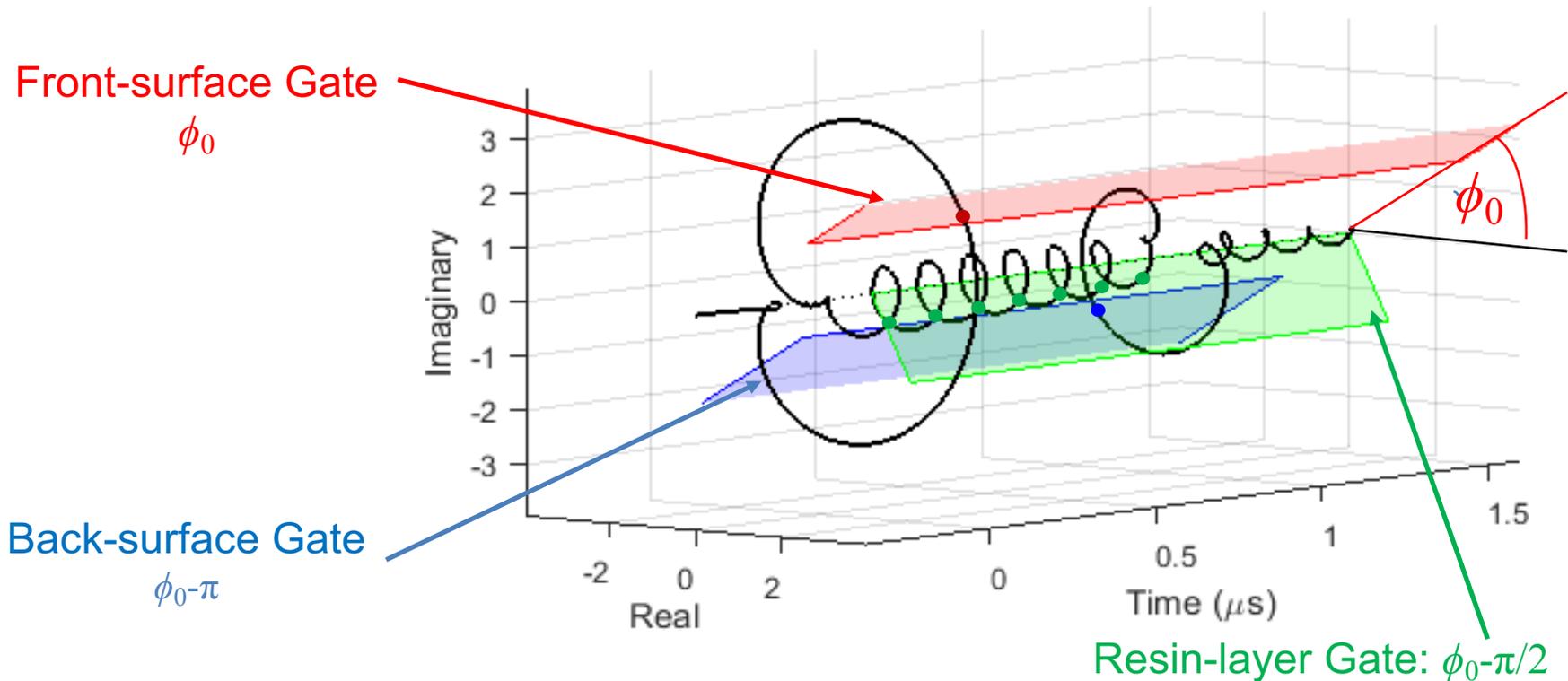


Stage 2: Ply tracking

- Immersion scan with input-pulse phase: $\phi_0 = \pi/6$
- Front locked at: ϕ_0 , back at: $\phi_0 - \pi$



- Immersion scan with input-pulse phase: $\phi_0 = \pi/6$
- Front at: ϕ_0 , back: $\phi_0 - \pi$, resin-layers: $\phi_0 - \pi/2$,



- Simulated ply drop, wrinkle and delamination

Simulation

Amplitude

Phase

Frequency

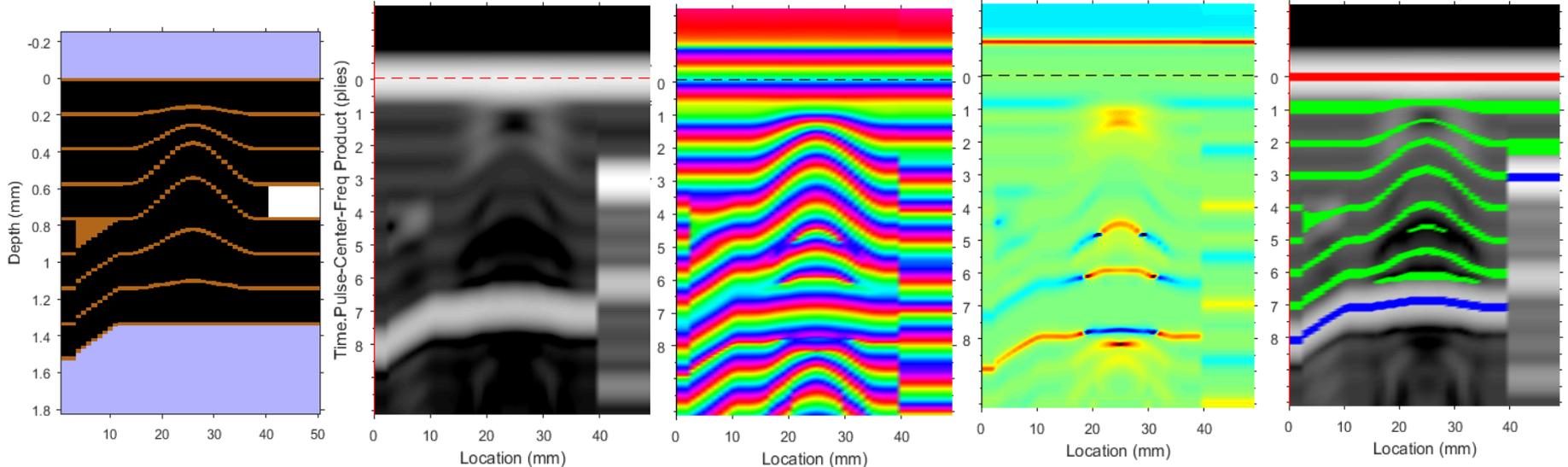
Ply Tracking

Instantaneous Amplitude (dB)
10 15 20 25 30 35

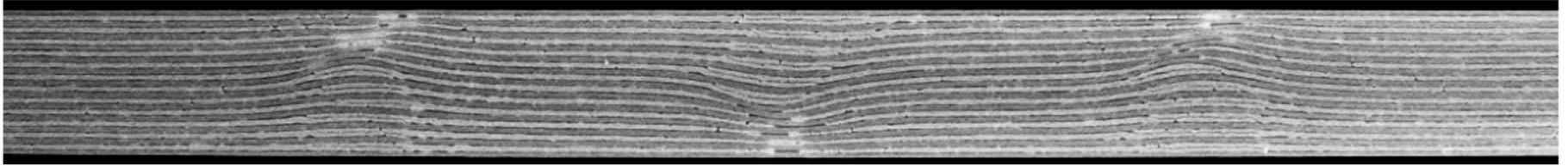
Instantaneous Phase (rad.)
-2 0 2

Instantaneous Frequency (MHz)
-10 0 10 20 30

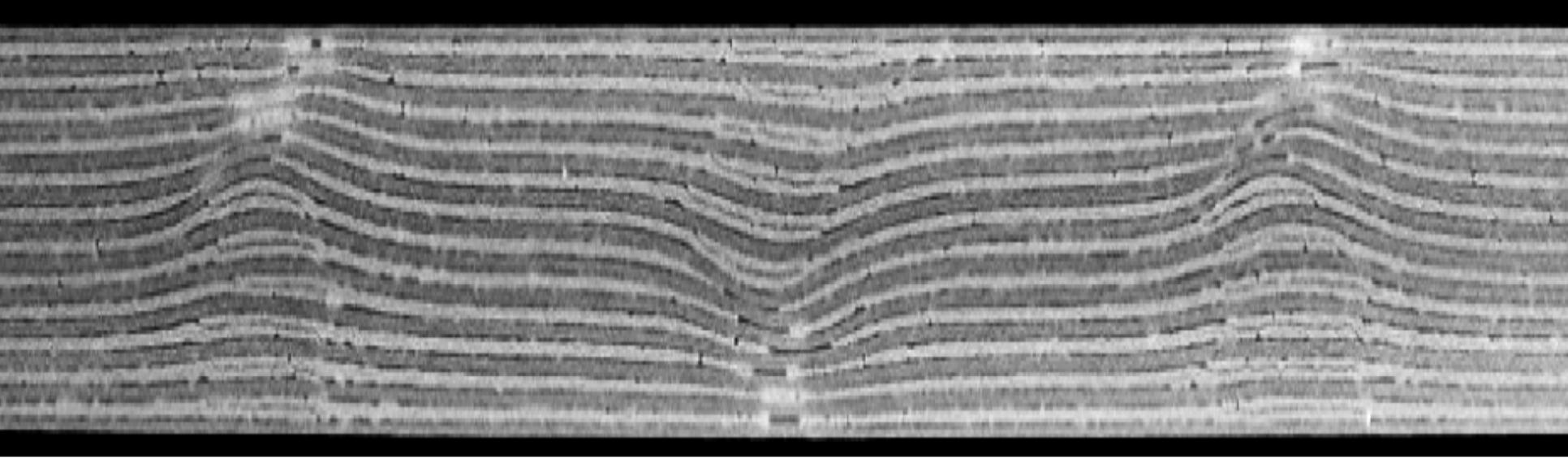
Instantaneous Amplitude (dB)
10 15 20 25 30 35



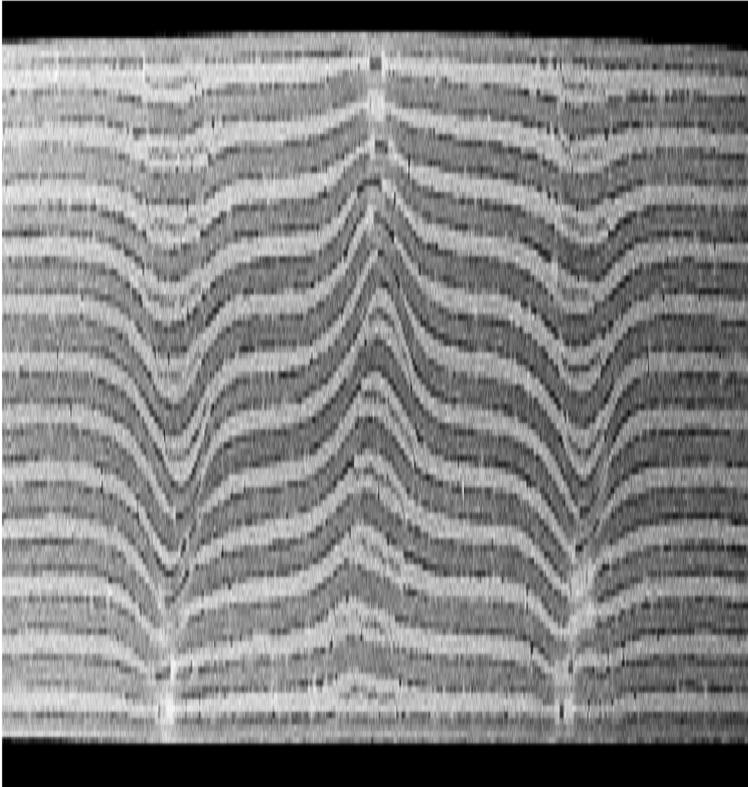
- Tape gaps and overlaps to cause wrinkling



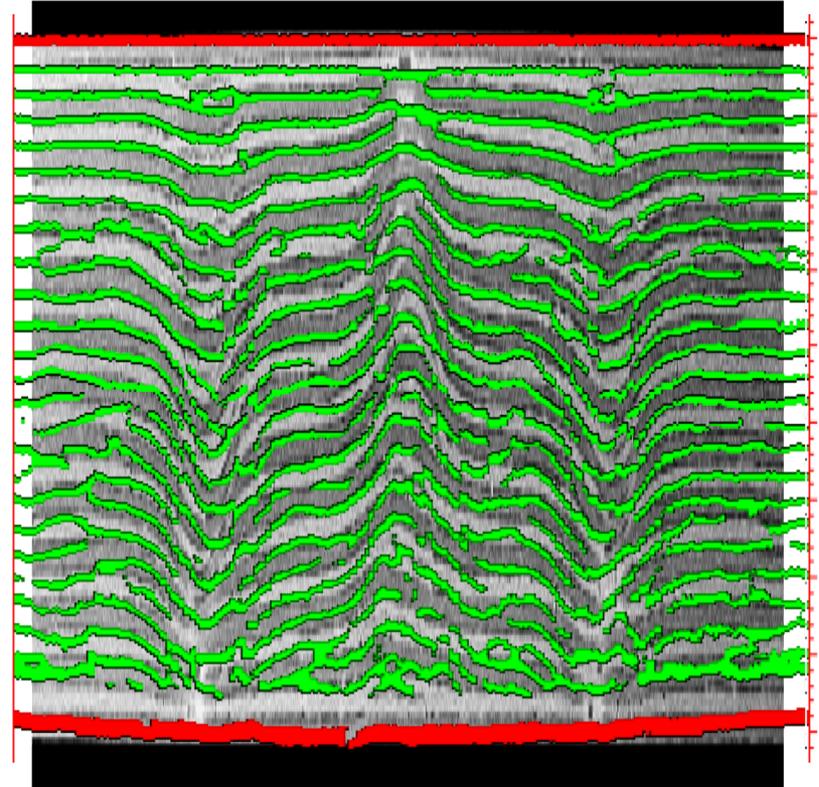
X-ray CT data



X-ray CT scan

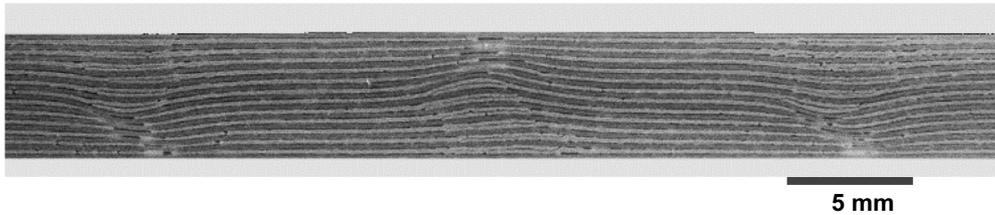


With ply-tracking overlay

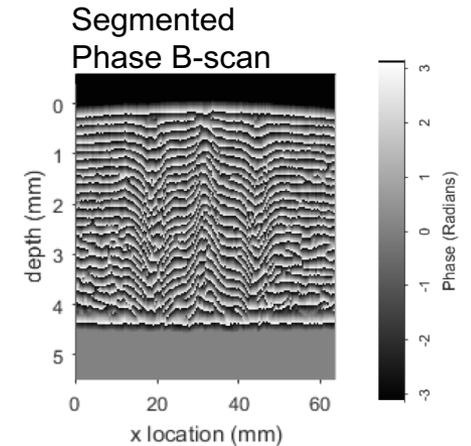
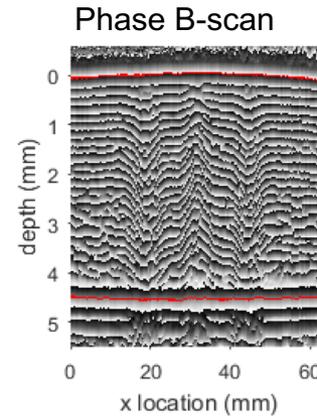
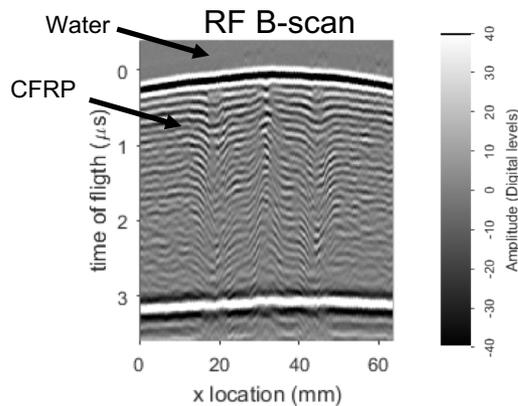


Stage 3: Ply Wrinkling

Validation by comparing ultrasonic-derived results to X-ray CT slices



X-ray CT of wrinkled test sample



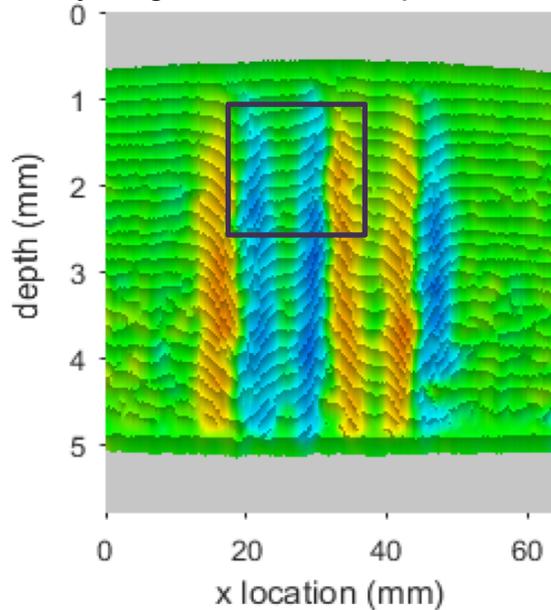
Identify front and back surface

Convert time to depth, taking into account the different velocities

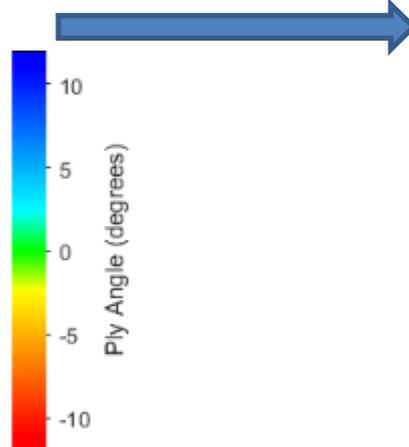
To retain true surface profile don't interface gate, fit a plane to the front surface

A **Structure Tensor** is used to determine gradients in the 3D phase

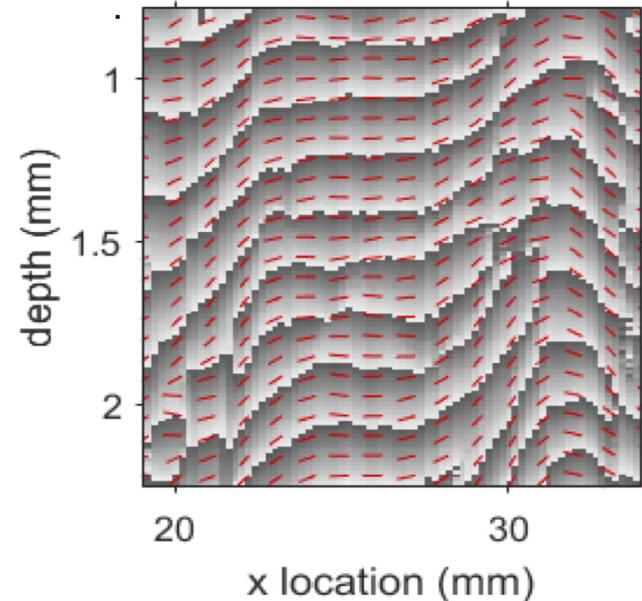
Ply angle overlaid on phase data.



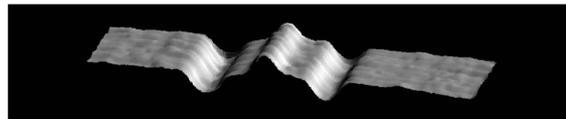
Do measurements
map to CT data?



Vector lines (red) overlaid on phase data



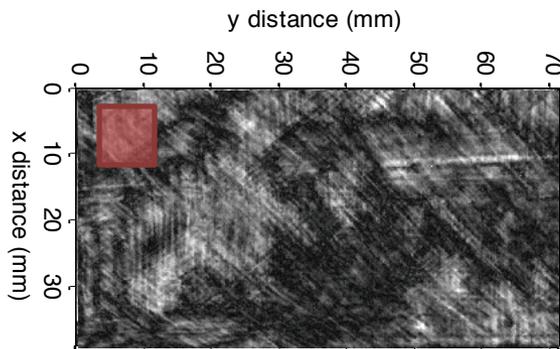
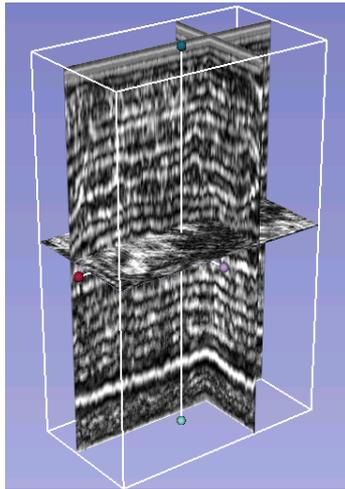
- 'Colours' look correct.
- More quantification required.



- Shows angles measurements accurately measure what is in the phase data

Stage 4: In-plane waviness, stacking sequence, 2D and 3D woven composites

- Use amplitude data



In-plane amplitude C-scan at depth = 1.4 mm
(approx. mid-laminate)

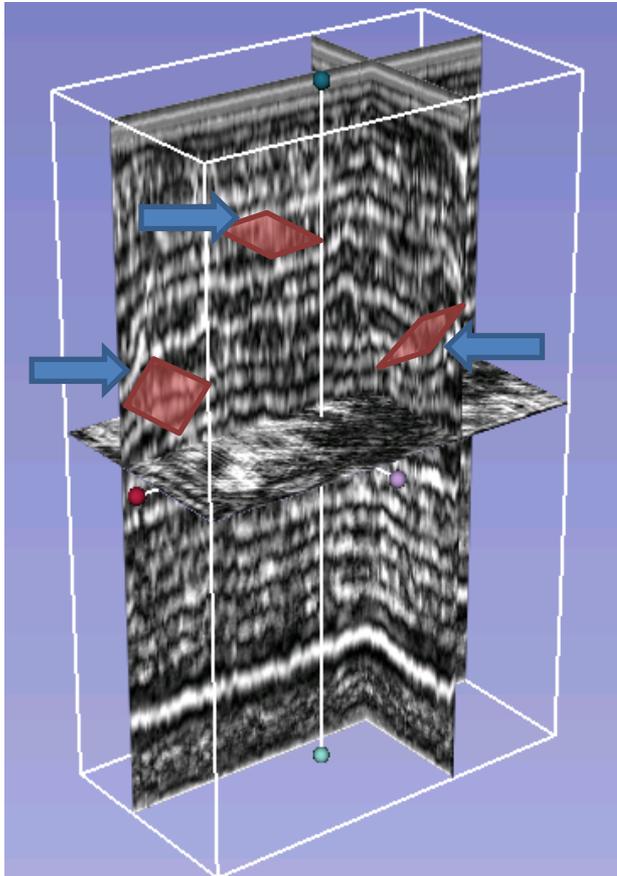
Fibre-tow sensitivity in ultrasound scan



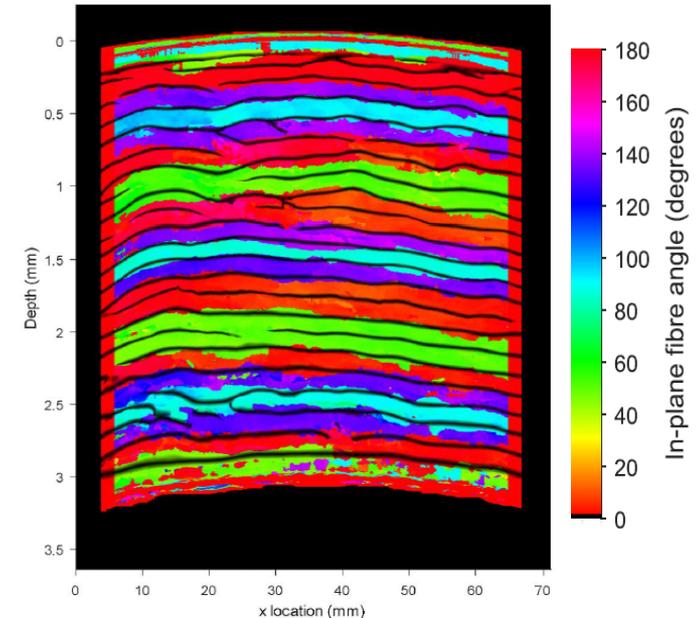
- Thickness variations in resin layers produce **amplitude** variations which track fibre tows.
- Need focused probe
 - Centre frequency and bandwidth at approximately the ply resonance frequency
 - -6dB Focal spot size less than tow width
- Analyse 2D region and step in raster scan.
- Build up a 2D fibre-angle orientation map.
- Step to next depth and repeat so we perform at every 3D pixel location.
- In regions with ply wrinkling, x-y slice is inappropriate

In-plane fibre orientation

A **Radon Transform** is used to measure the dominant fibre-tow angle.

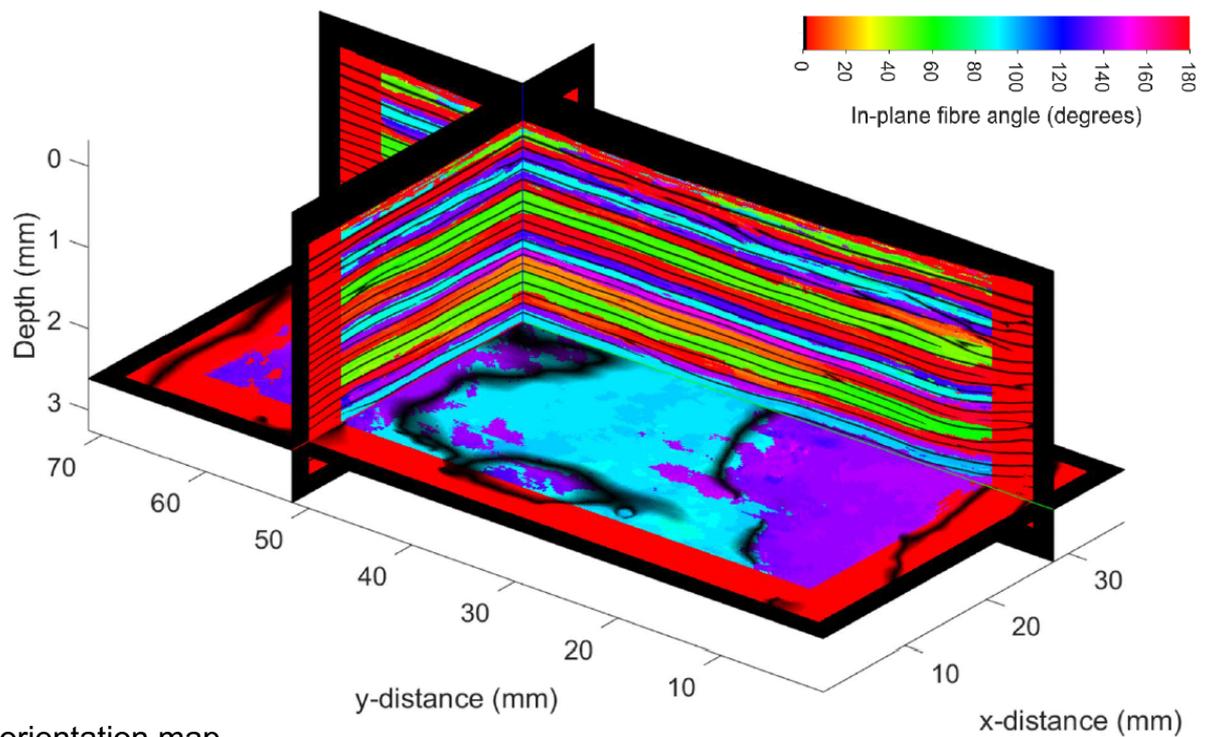


- We can measure the PLY orientation
- Since fibres are constrained to plies, use ply orientation to guide our 2D processing
- Perform at every 3D pixel location
- Smooth the phase data 'aligned to plies'



- Cross section with phase-derived ply-location overlay
- Shows double plies

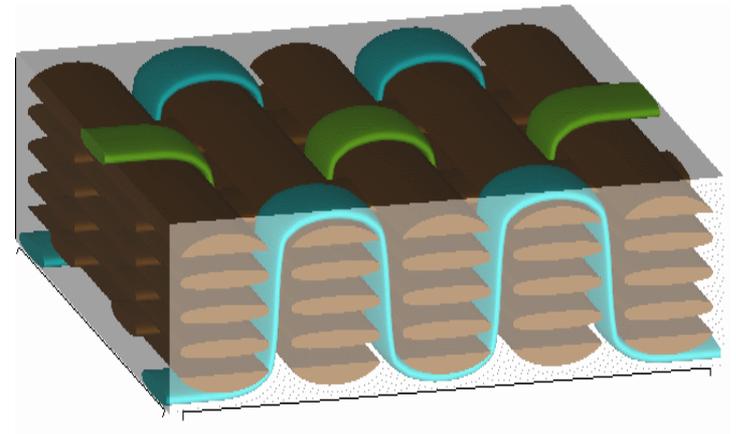
Fibre orientation Results



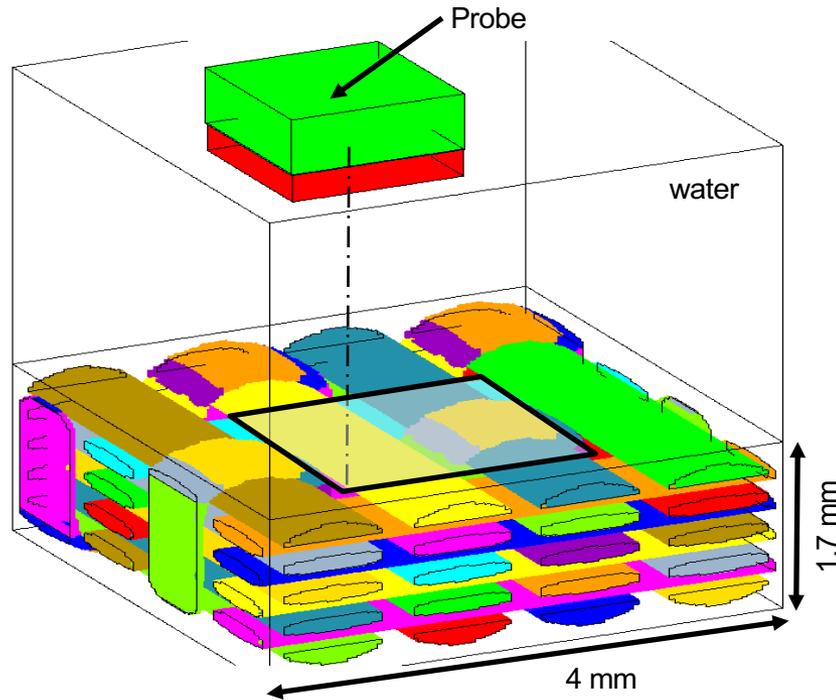
3D In-plane fibre orientation map

3D Woven Composites

Orthogonal weave example



OnScale (PZFlex) Model

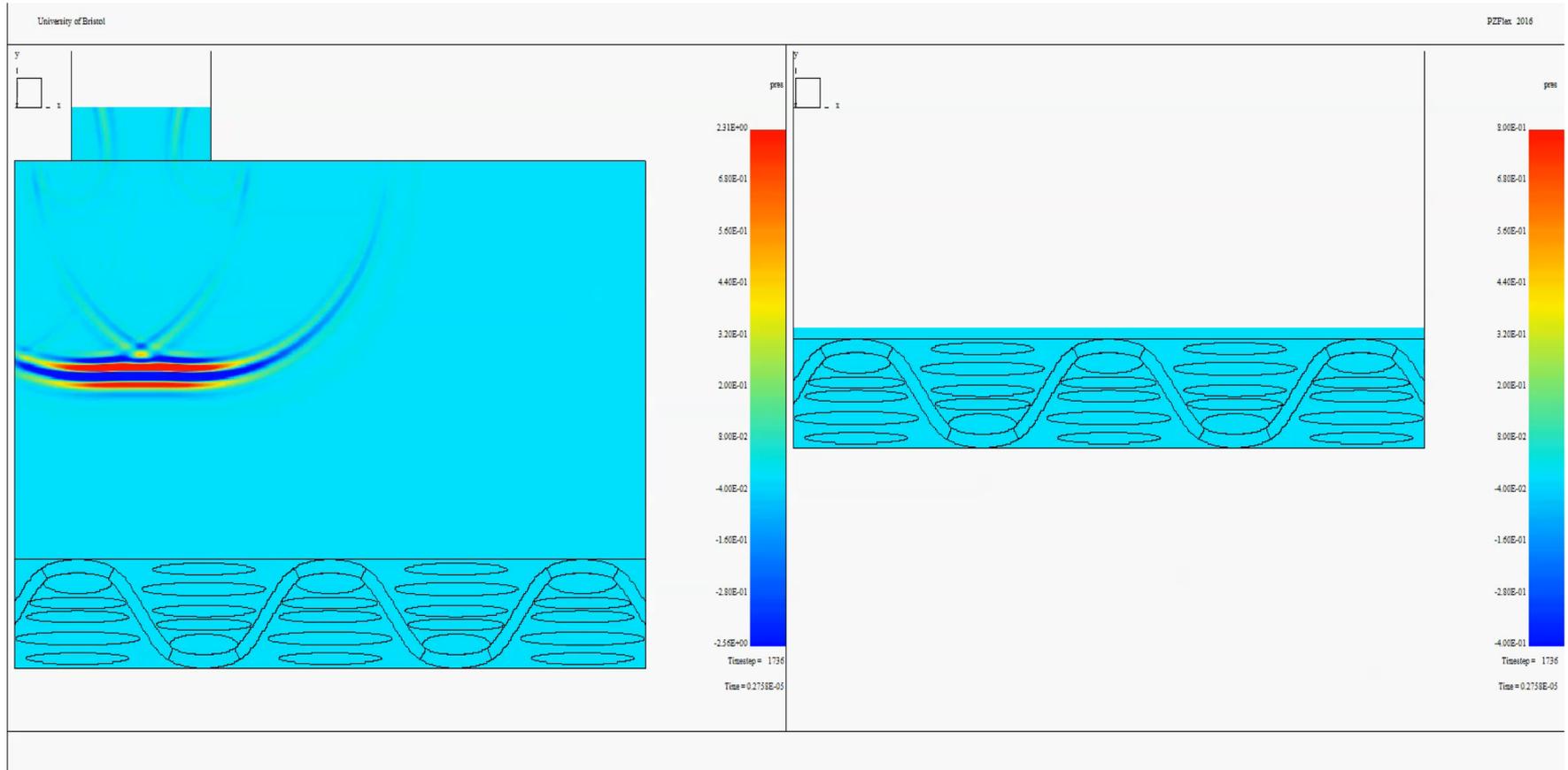


6 regions (yarns 0, 1, 4, 5, 6, 9)
with different velocities

6	1	6	1	6	1	6
5	0	5	0	5	0	5
9	4	9	4	9	4	9
5	0	5	0	5	0	5
6	1	6	1	6	1	6
5	0	5	0	5	0	5
9	4	9	4	9	4	9
5	0	5	0	5	0	5
6	1	6	1	6	1	6

Each fibre orientation
has a different color in
PZFlex

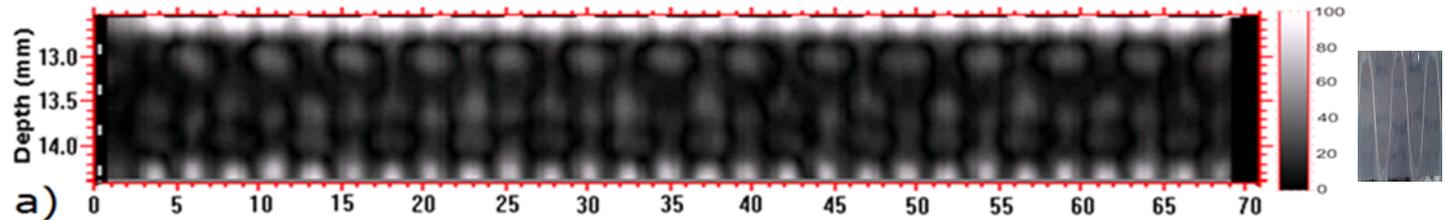
Binding-yarn effect from FE modelling



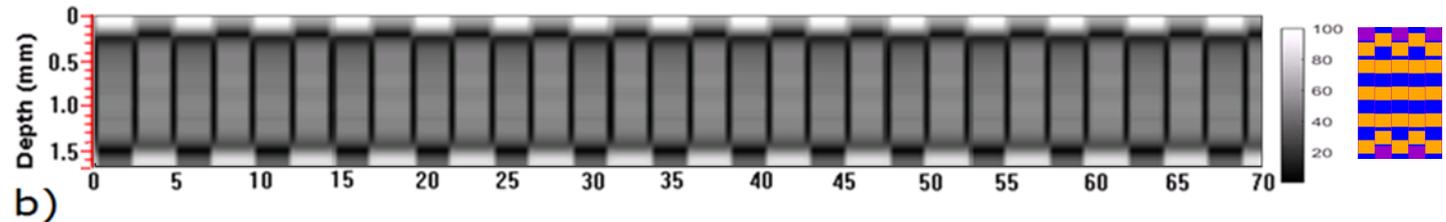


Binder-yarn region: 5 MHz Instantaneous. amplitude

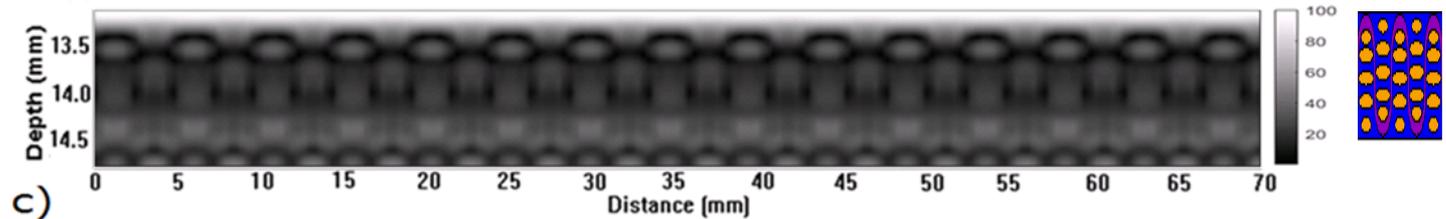
Experiment:



Analytical model:



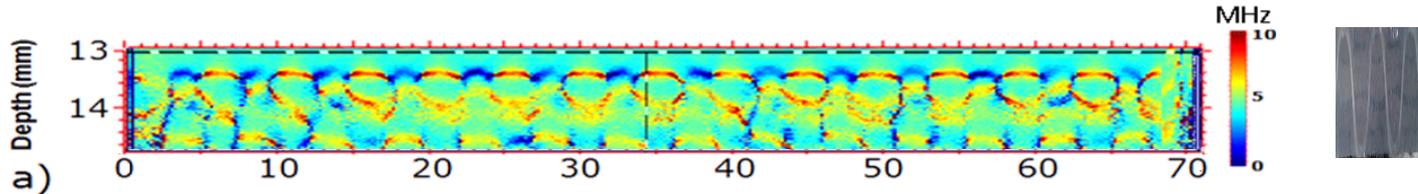
Finite Element model:



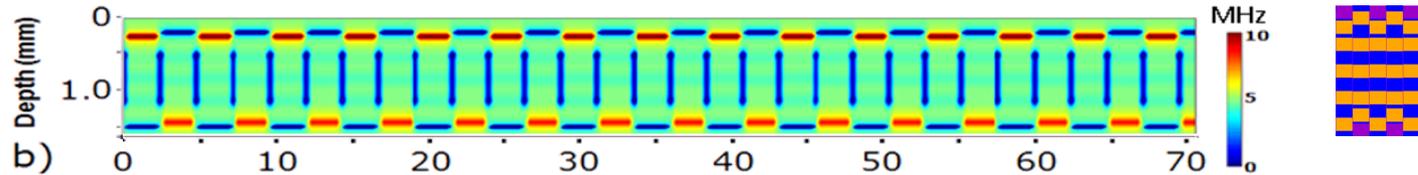
6	1	6	1	6	1	6
5	0	5	0	5	0	5
9	4	9	4	9	4	9
5	0	5	0	5	0	5
6	1	6	1	6	1	6
5	0	5	0	5	0	5
9	4	9	4	9	4	9
5	0	5	0	5	0	5
6	1	6	1	6	1	6

Binder-yarn region: 5 MHz Instantaneous frequency

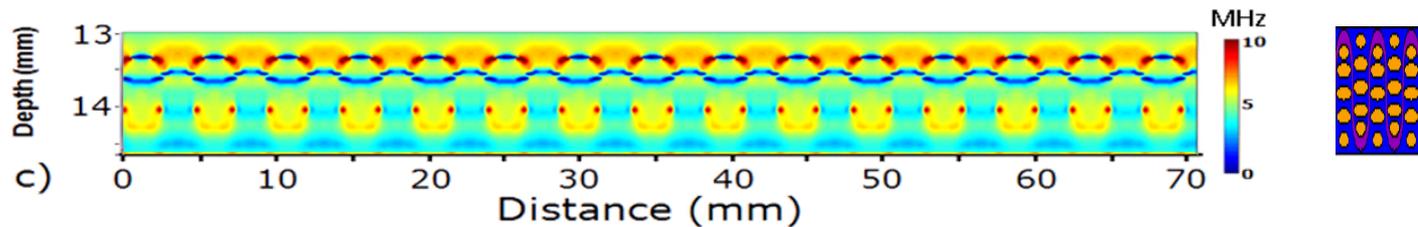
Experiment:



Analytical model:

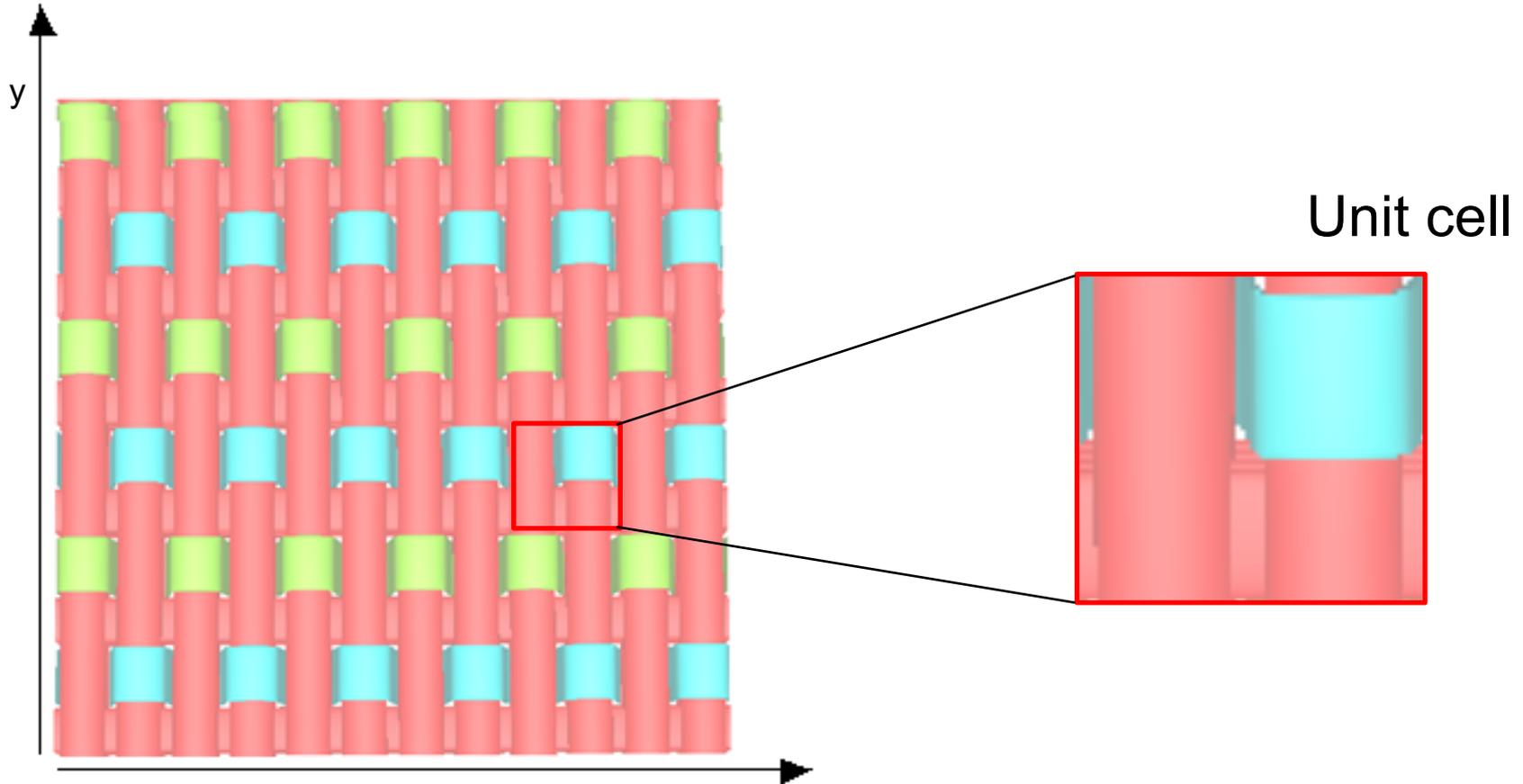


Finite Element model:



Conclusion: Level of compaction is important in modelling & in practice

The Unit Cell



Unit cell is the smallest repetitive element in 2D or 3D

In-plane Benchmark Subtraction technique

For each depth below the surface, use the in-plane C-scan...

- Create a 'benchmark' pristine scan using a unit cell and cross-correlation in 2D
- Subtract the benchmark scan from the actual measured scan

Use of the instantaneous amplitude for these results, but should also work with instantaneous frequency

Method demonstrated using FE data, then applied to experimental data...